

# Kinetic modelling of kerogen cracking during oil shale process : **influence of organic matter source**

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**F. Behar and P. Allix**



# General outline

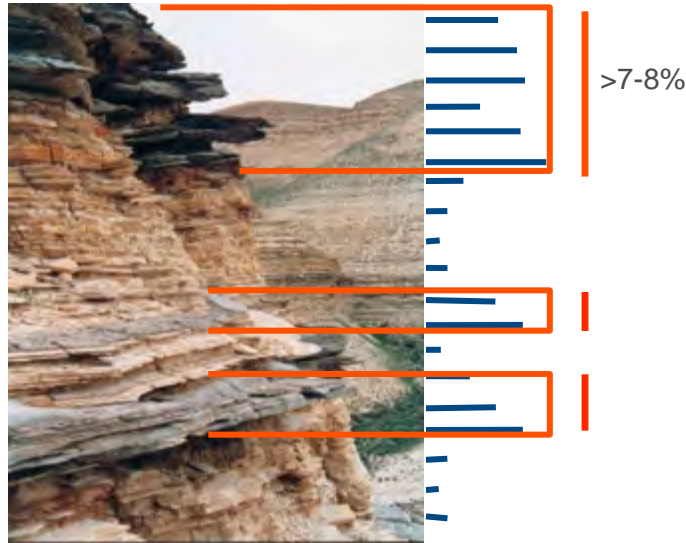
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- ▶ **I – Introduction**
- ▶ **II – Kerogen characterization**
  - Definition of the main organic matter
    - Initial geological deposit
    - Oil shale potential
- ▶ **III – Understanding the main reaction of kerogen cracking**
  - Kinetic schema
  - Micro pilot reactor
  - Mass balances
  - Compositional model
- ▶ **IV – Impact on oil shale yield and chemical composition**
  - Primary products
  - Secondary reaction
- ▶ **V – Conclusions**

# Oil shale pyrolysis : new challenges for unconventional resources

Solid organic matter (kerogen)

Total Organic Carbon



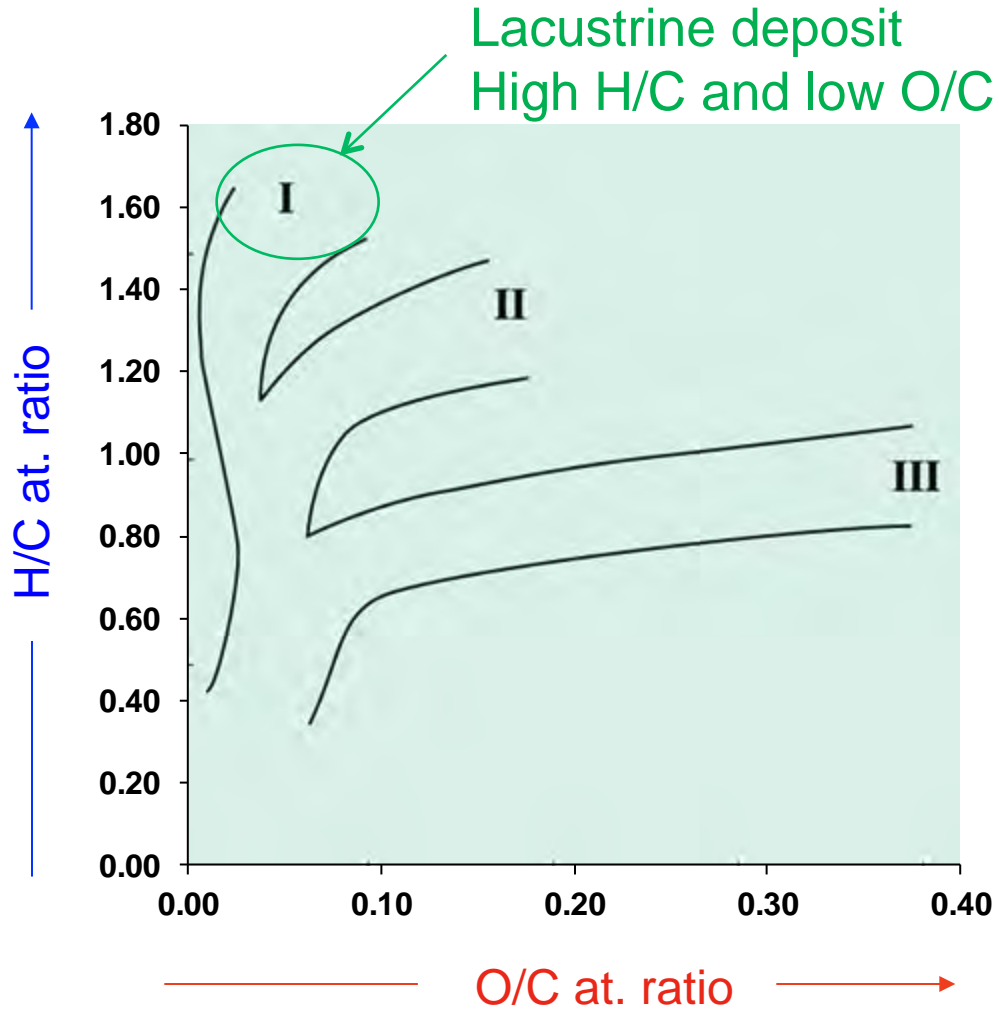
Oil shale process  
T : 200 to 400°C  
Weeks to months



°API > 30

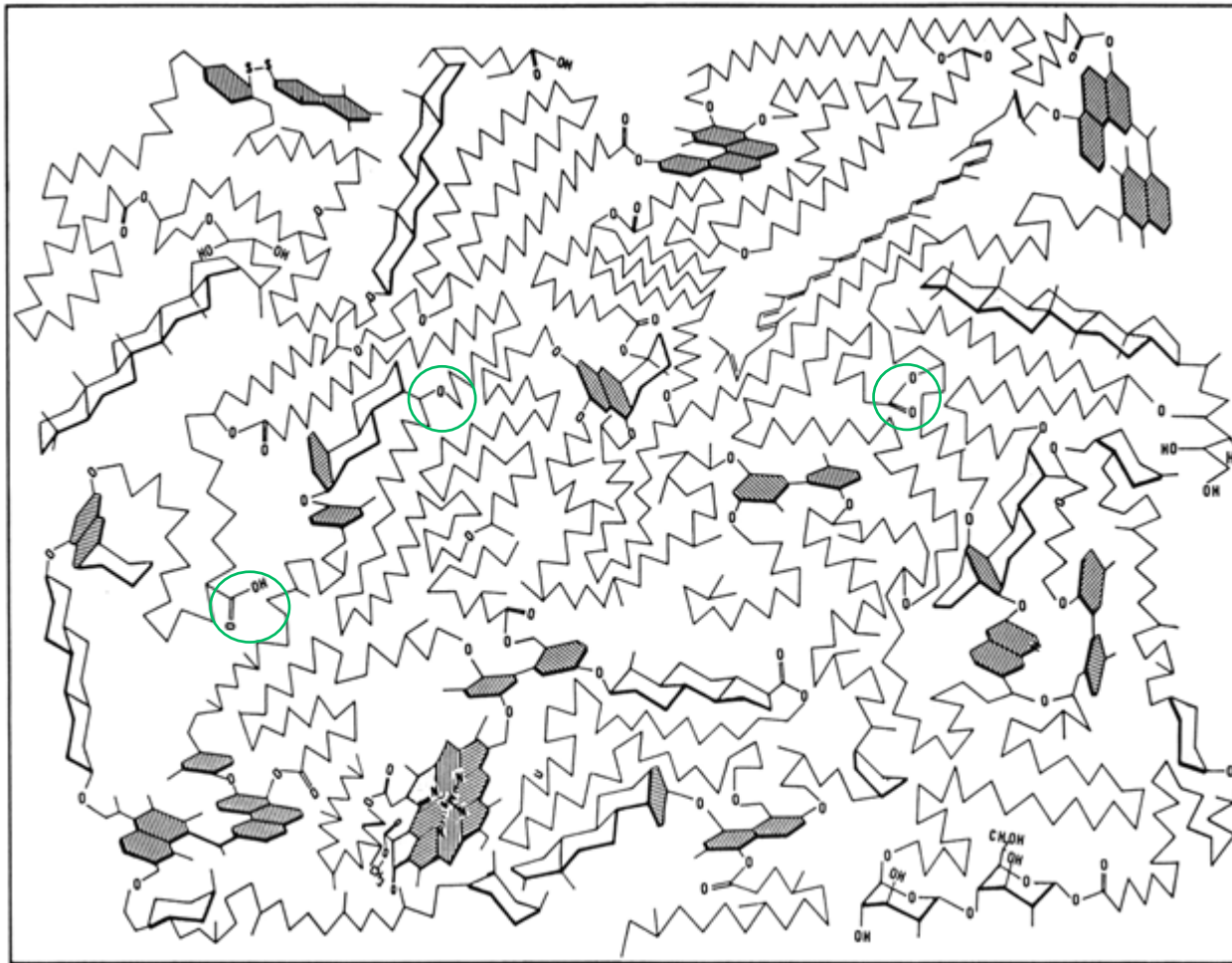
How does organic matter quality impact **yield** and **chemical composition** of the produced oil ?

# Classification of organic matter in source rocks



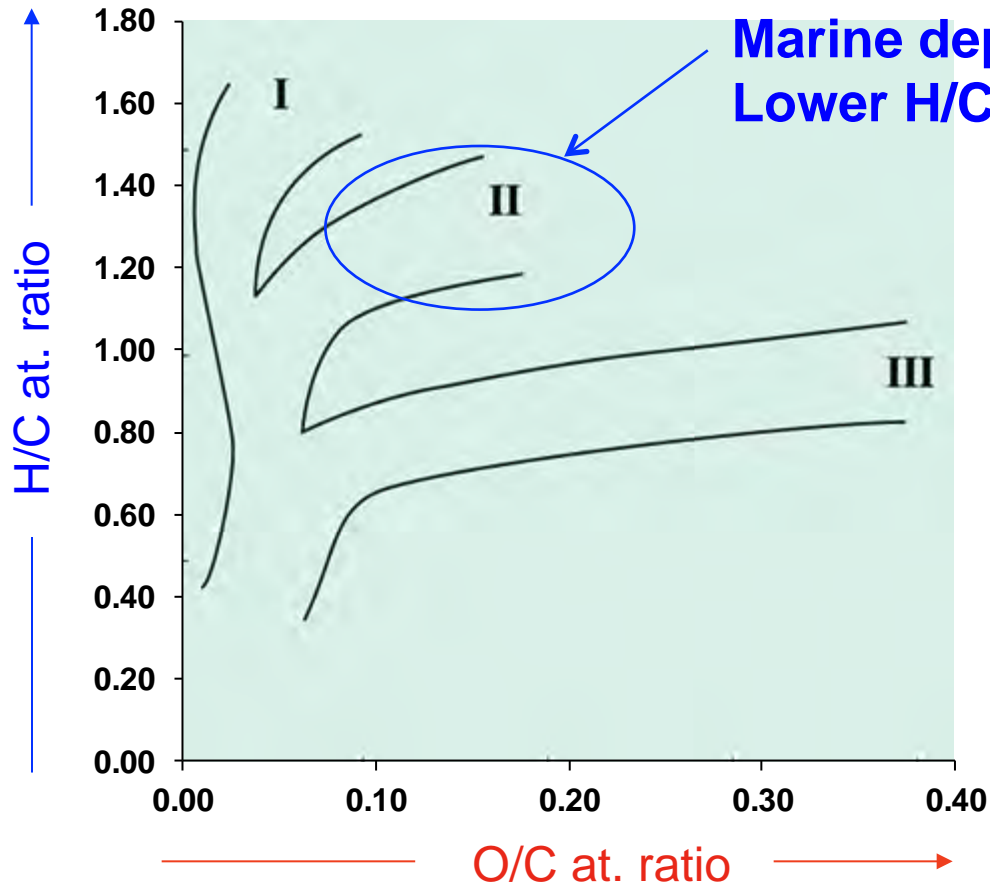
Van Krevelen diagram

# Classification of organic matter in source rocks



Aliphatic chains  
Low aromatic content  
Ester – Acids – Ether

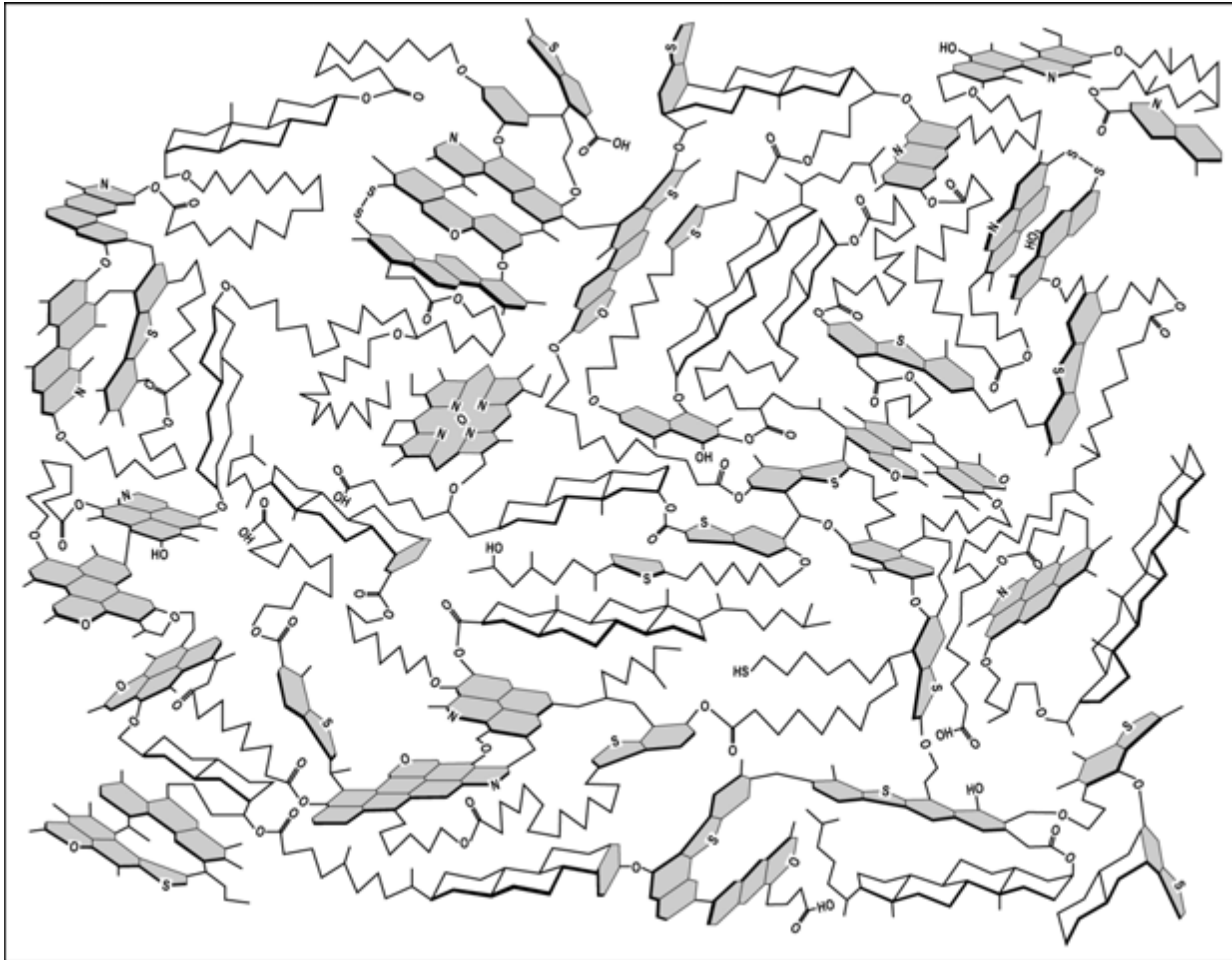
# Classification of organic matter in source rocks



Marine deposit  
Lower H/C and higher O/C

Van Krevelen diagram

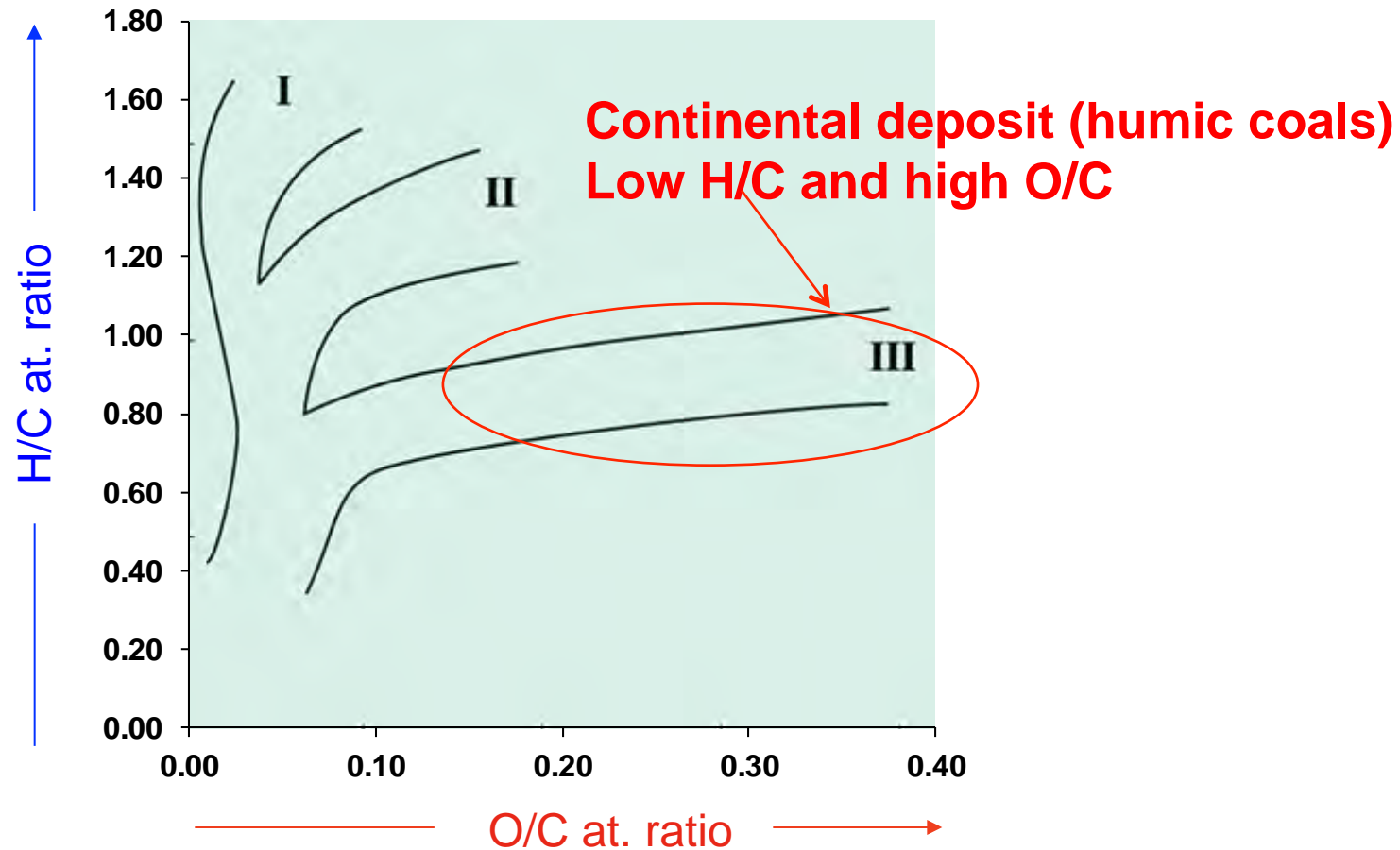
# Chemical structure of marine organic matter (Type II)



**Aliphatic chains and cyclanes**  
**Significant aromatic content**  
**Ester – Acids – Ether**

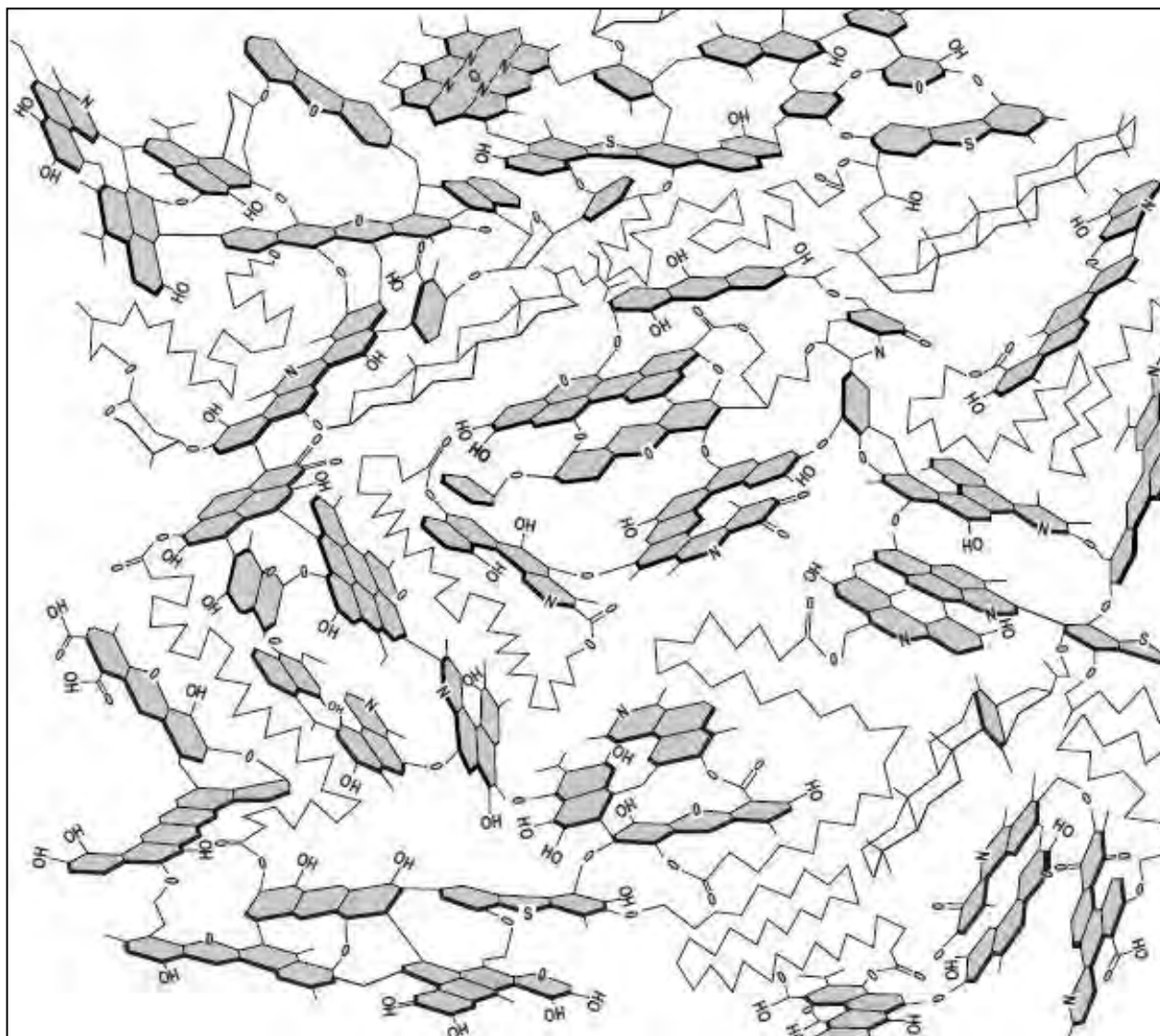
**Type II – S**  
**High sulfur content**  
**Confined marine deposit**

# Classification of organic matter in source rocks





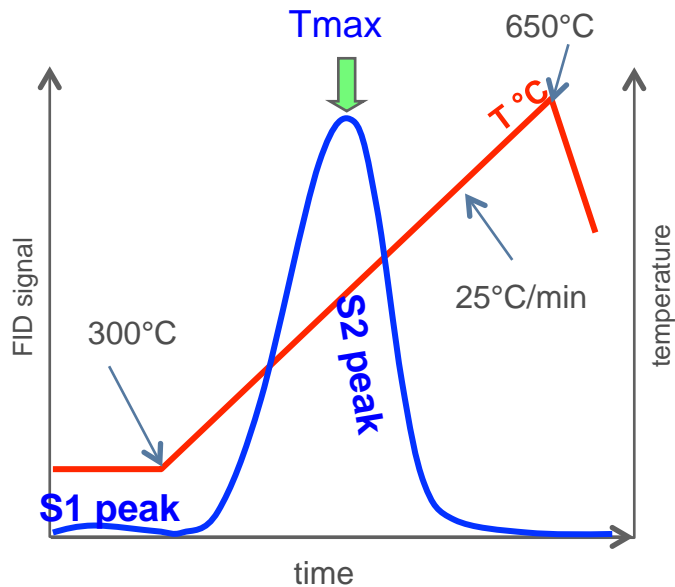
# Chemical structure of continental organic matter (Type III)



**Aromatics and phenols**  
**Ester – Acids – Ether**

# Shale oil potential

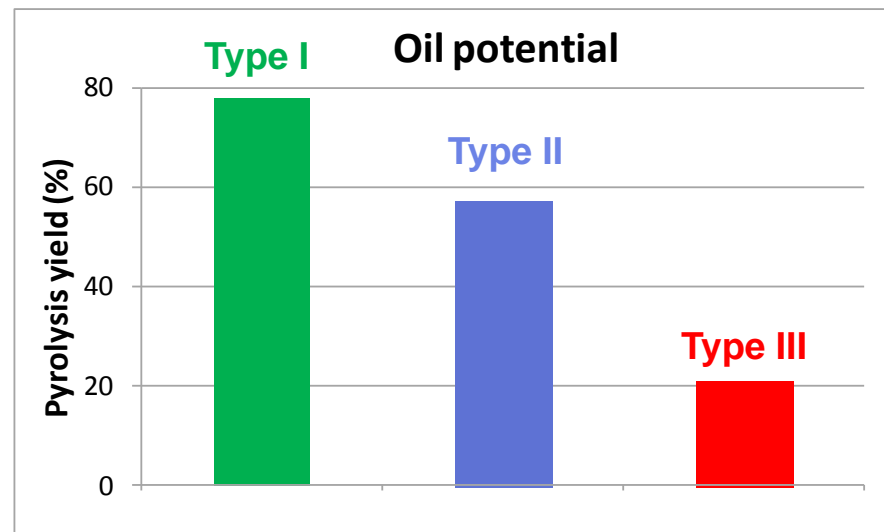
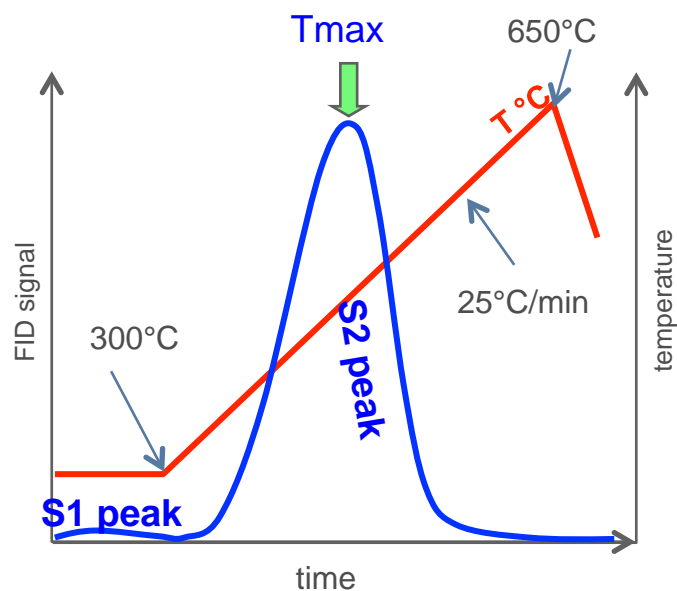
## Rock Eval pyrolysis



At 650°C : 100% kerogen conversion  
→ S2 = maximum yield

# Shale oil potential

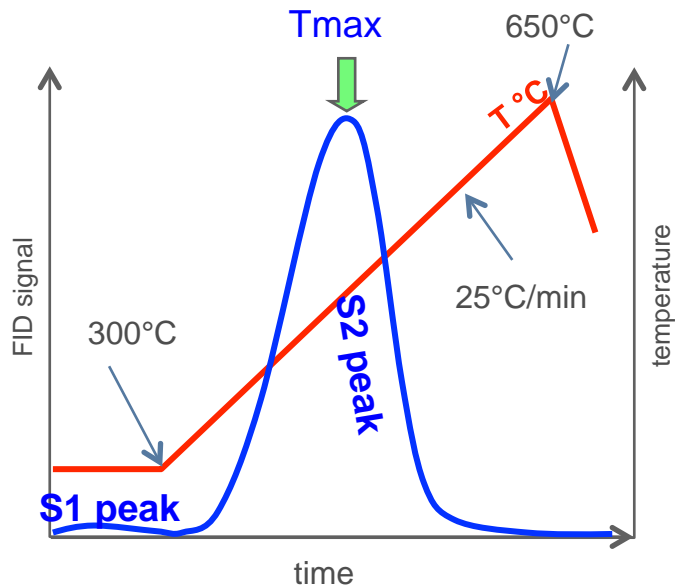
## Rock Eval pyrolysis



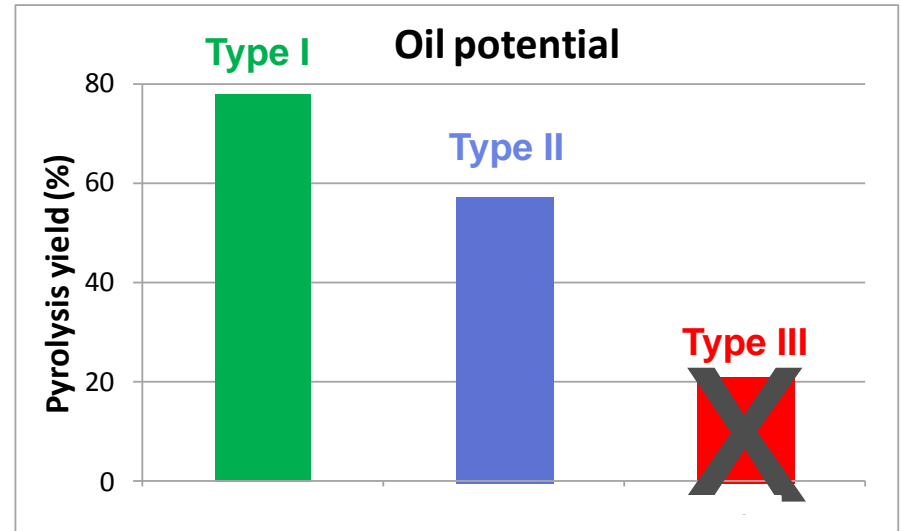
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# Shale oil potential : f (organic matter type)

## Rock Eval pyrolysis



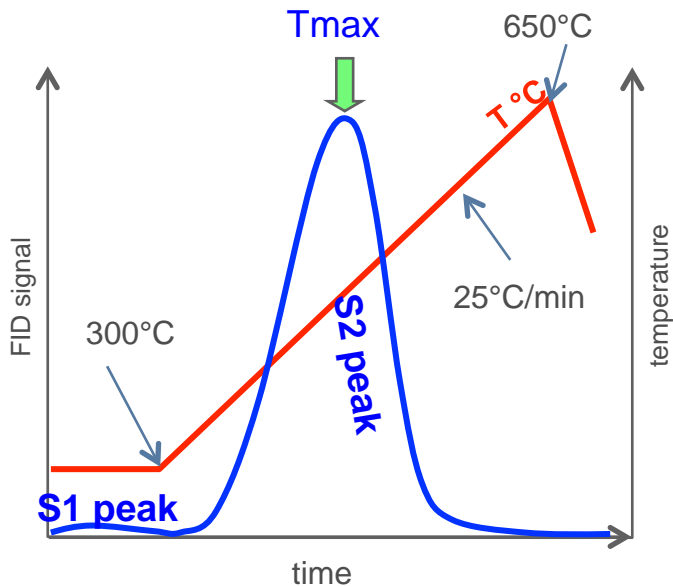
At 650°C : 100% kerogen conversion  
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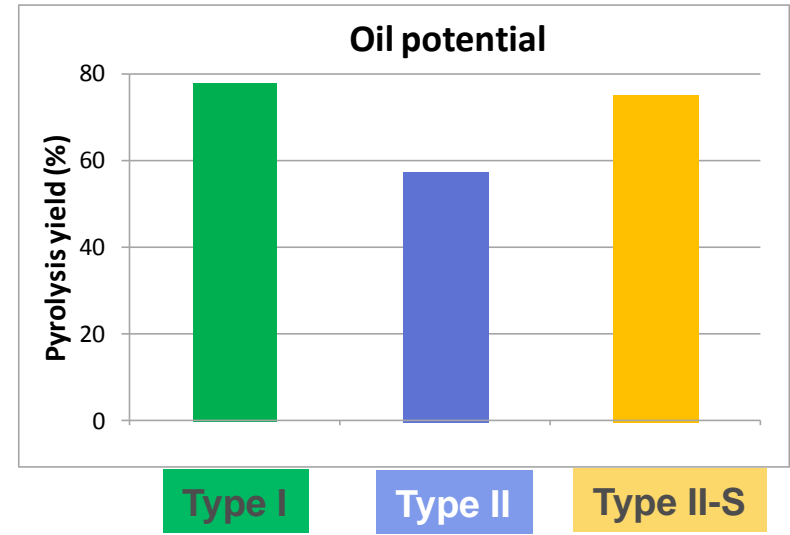
Oil shale pyrolysis :  
Type I and II are good candidates

# Shale oil potential : f (organic matter type)

## Rock Eval pyrolysis



At 650°C : 100% kerogen conversion  
→ S2 = maximum yield



Oil shale pyrolysis :  
Type I, II and II – S are good candidates

# General outline

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## ► I – Introduction

## ► II – Kerogen characterization

- Definition of the main organic matter source
  - Initial geological deposit
  - Oil shale potential

## ► III – Understanding the main reaction of kerogen cracking

- Kinetic schema
- Micro pilot reactor
- Mass balances
- Compositional model

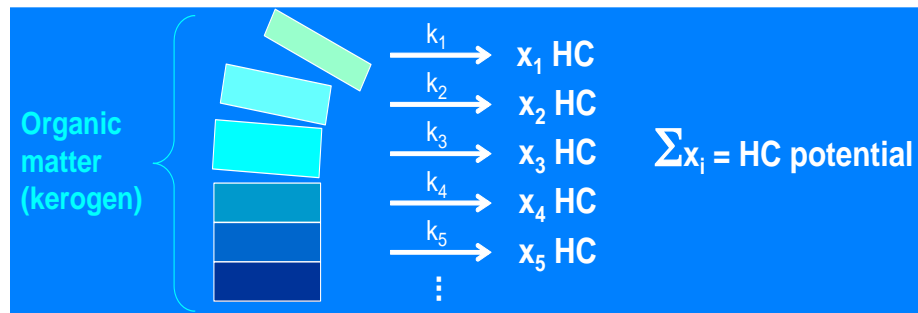
## ► IV – Impact on oil shale yield and chemical composition

- Primary products
- Secondary reaction

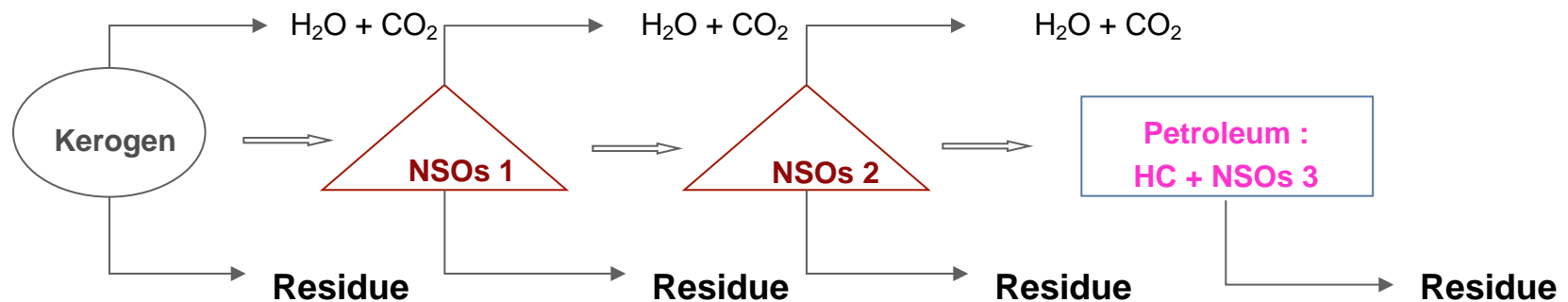
## ► V – Conclusions

# Two types of kinetic schema for kerogen cracking

I – Parallel reactions : hydrocarbons are primary products  
(Burnham and Brown 1987; Ungerer, 1991...)



II – Successive reactions : HC are not directly generated from kerogen  
(Fitzgerald and van Krevelen, 1959, Tissot, 1969, Lewan 1983, Behar et al., 2008...)



**NSOs 1 and 2 = Asp + Resins**

# Kerogen cracking in laboratory conditions

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## ► Open system pyrolysis

- Generated asphaltenes are cracked and not vaporised
- HC potential from asphaltenes cannot be quantified
- Only apparent kinetic schema : parallel reactions

## ► Closed pyrolysis system

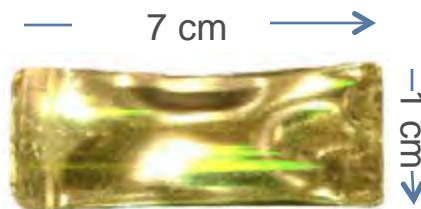
- Generated asphaltenes recovered by solvent extraction
- Kinetics of asphaltenes generation and cracking
- Discriminate between parallel and successive kinetic schema



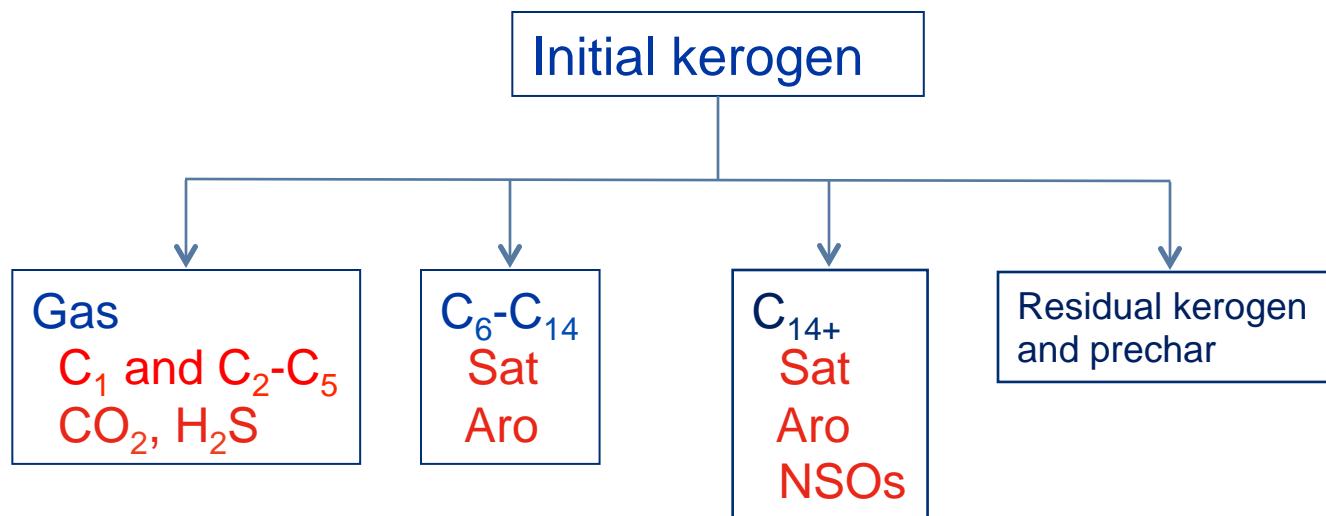
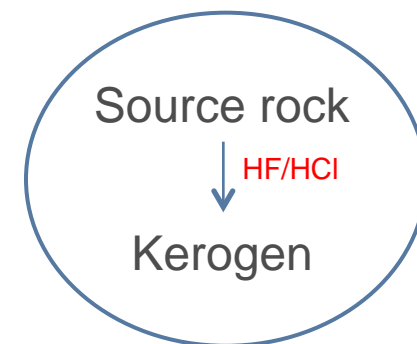
# Micro reactor : analytical workflow

## Pyrolysis experiments:

Sealed gold tubes  
300 – 400°C  
1 week to 6 months

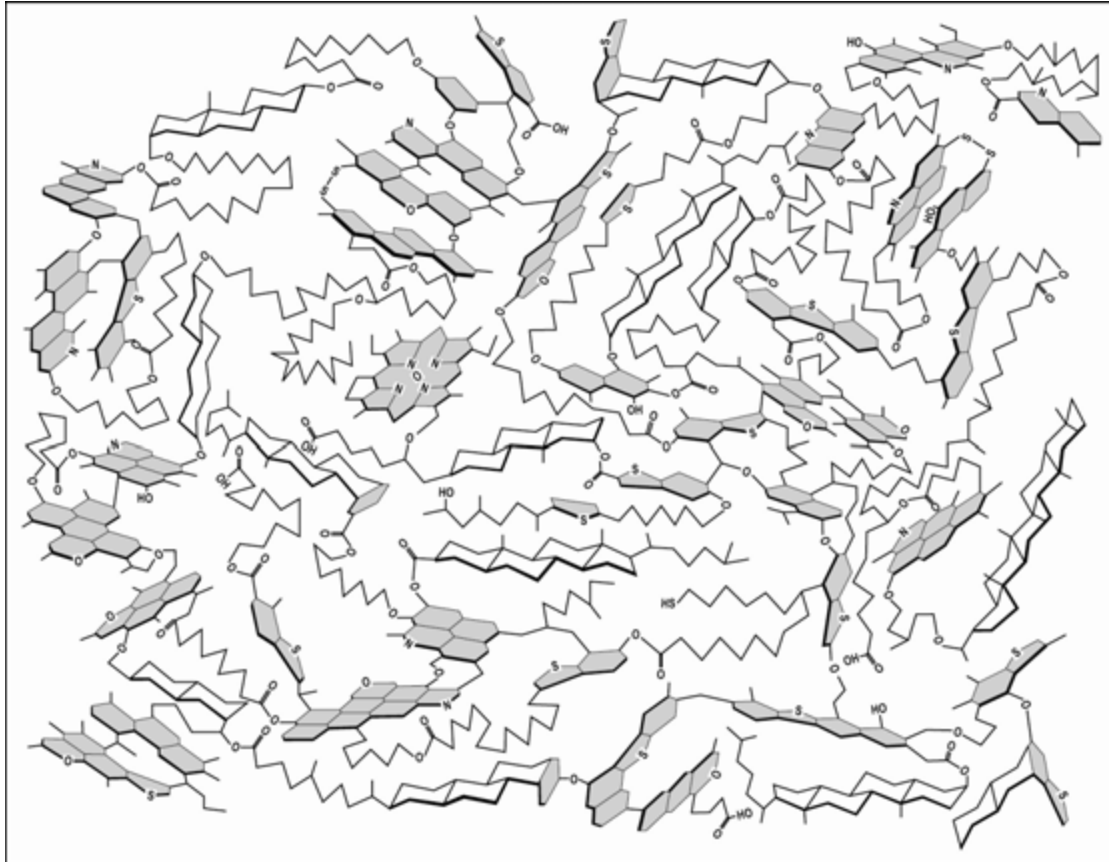


Kerogen amount : 250 mg – 4 g



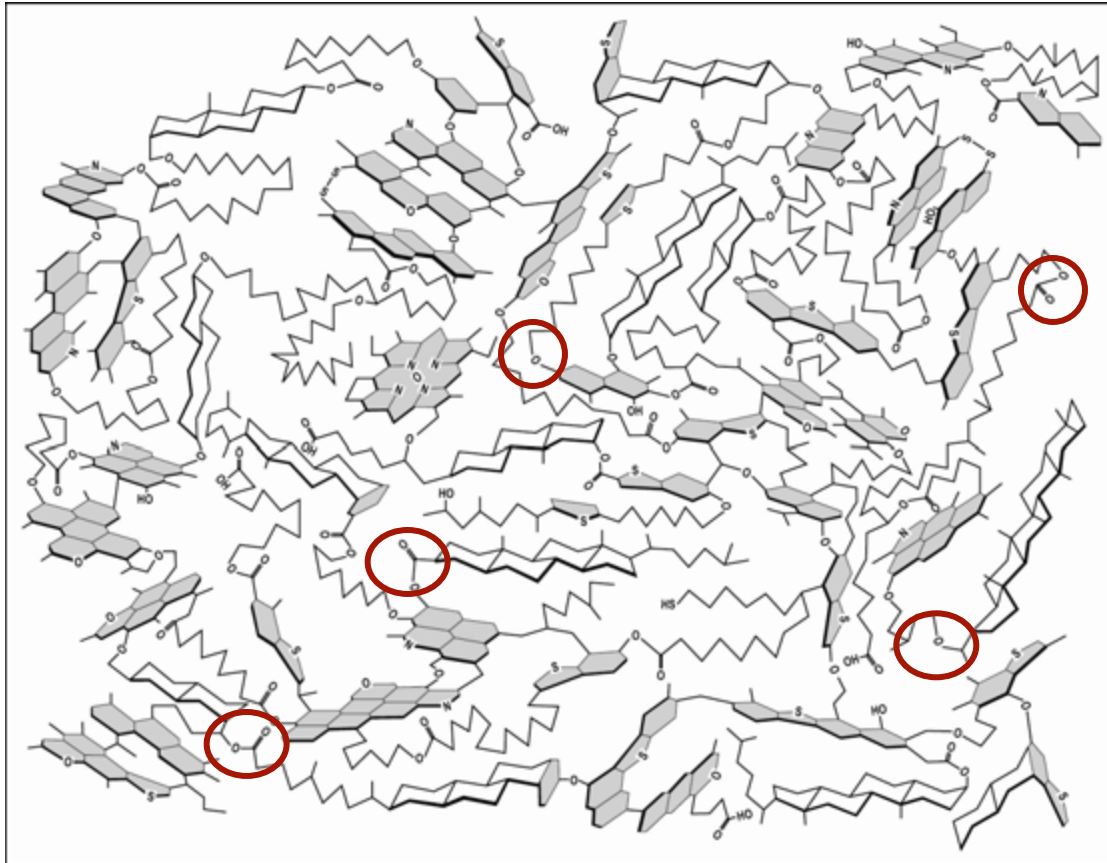
gas + liquid + solid > 95%

# Thermal cracking of kerogen



- Complex molecule of high molecular weight
- Functional groups between kerogen moieties

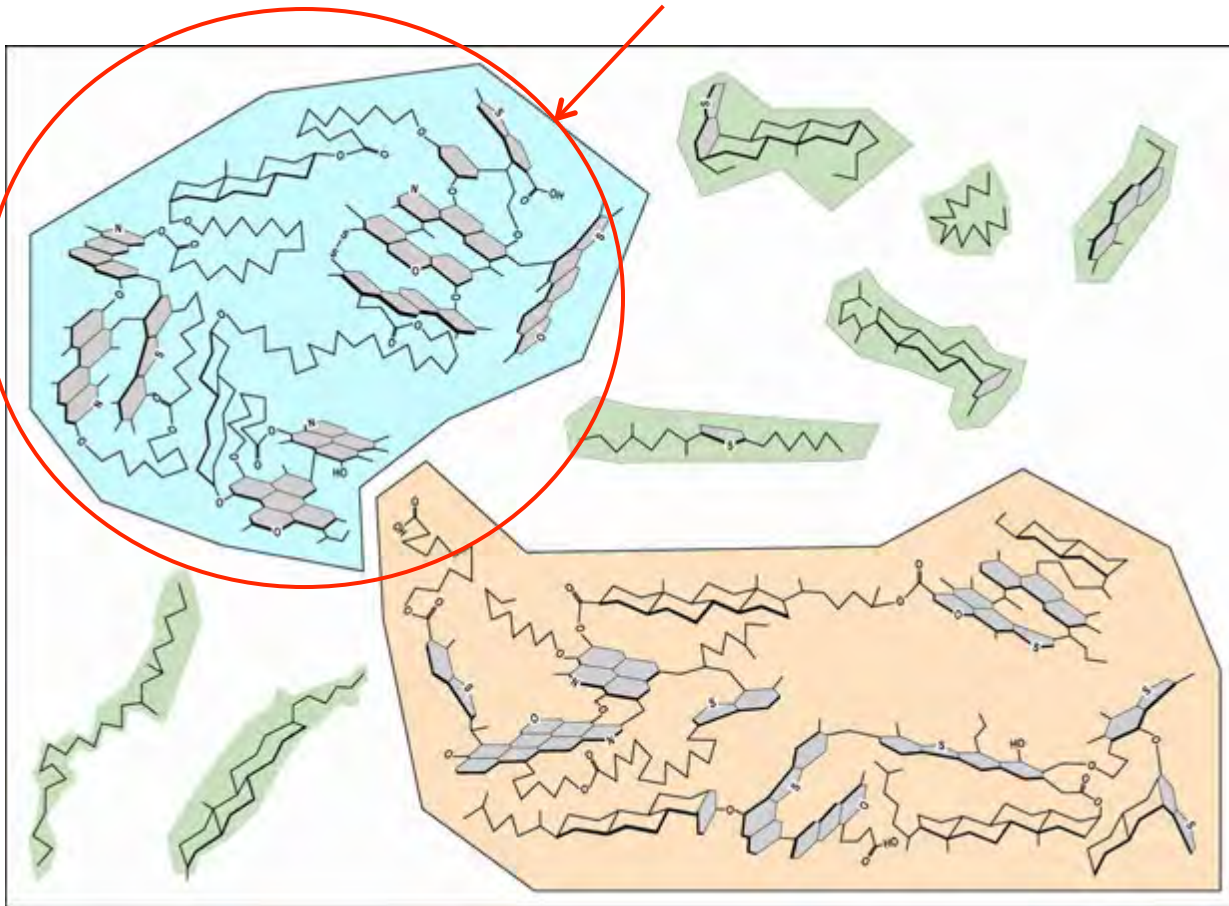
# Thermal cracking of kerogen



Thermal cracking  
of functional groups

# Liquid products : asphaltenes and HC

**Asphaltenes**

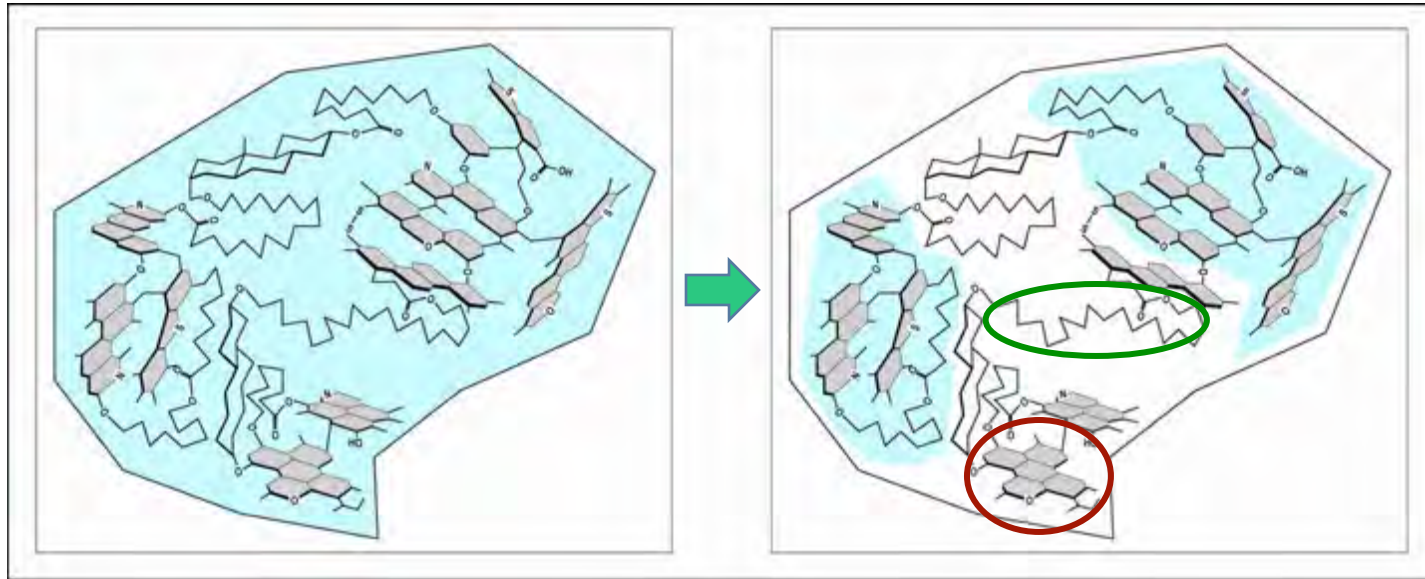


kerogen



Asphaltenes  
First source of HC (1)

# Asphaltenes cracking : resins generation



**Asphaltenes**



**Resins + HC2**

**Asphaltenes**



**Char precursor**

# HC generation : 3 main reactions

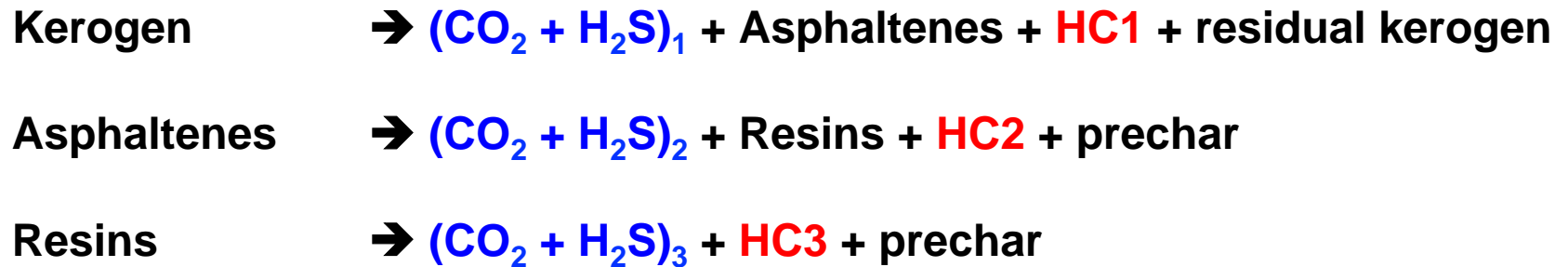
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**Kerogen** →  $(\text{CO}_2 + \text{H}_2\text{S})_1$  + Asphaltenes + **HC1** + residual kerogen

**Asphaltenes** →  $(\text{CO}_2 + \text{H}_2\text{S})_2$  + Resins + **HC2** + prechar

**Resins** →  $(\text{CO}_2 + \text{H}_2\text{S})_3$  + **HC3** + prechar

# HC generation : 3 main reactions



Oil shale pyrolysis

2 main steps for hydrocarbon production

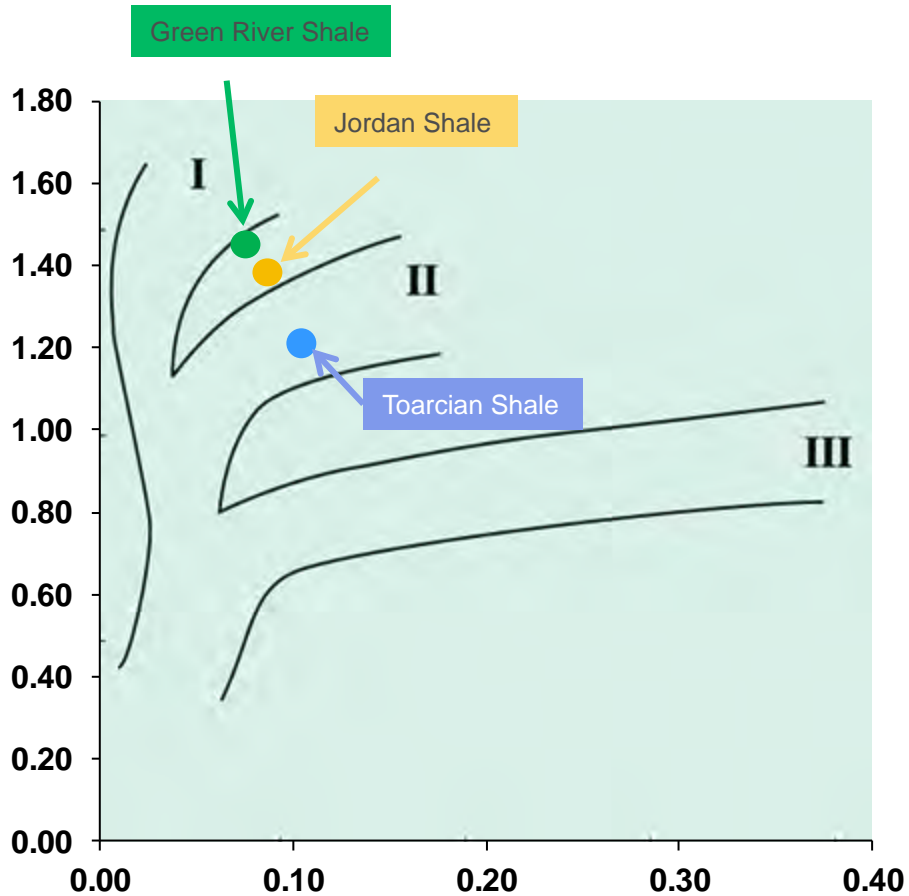
1 – Cracking of **non mobile compounds** (kero + asp + res.)

2 – Partial cracking of the **mobile compounds** (*resins* and HC)

Results on 3 selected oil shales

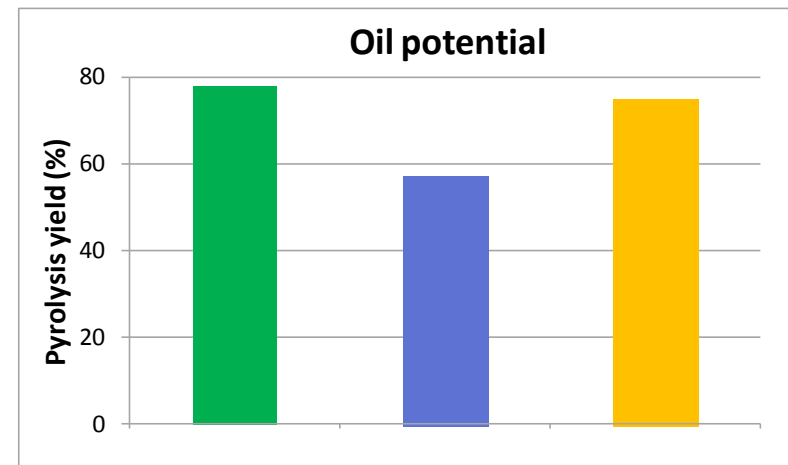


# Results on 3 selected oil shales



Type I lacustrine : Green River Shale (USA)  
 Type II marine : Toarcian Shale (France)  
 Type II-S marine : Jordan Shale (Jordanie)

Oil shale potential : 300-600°C at 25°C/min



Type I

S = 0.7%

Type II

S = 3.1%

Type II-S

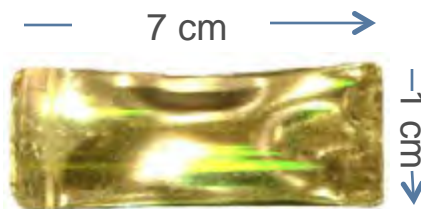
S = 12.9%



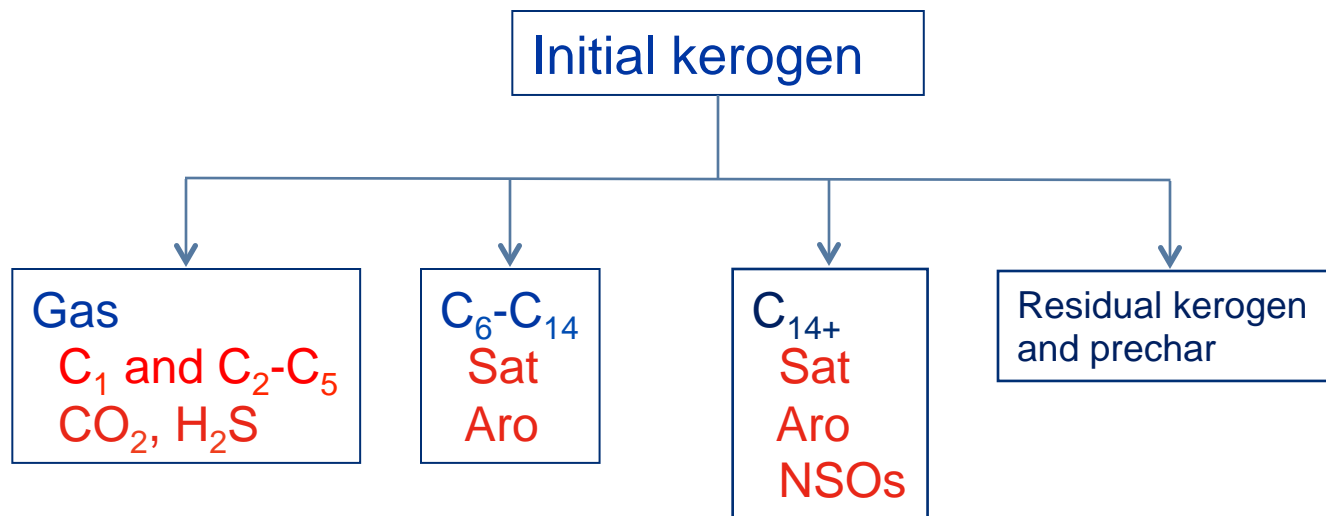


# Experimental simulation in closed micro reactor

**T = 325°C**  
**time from 1 to 216h**



Initial amount : 250 mg – 4 g

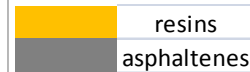
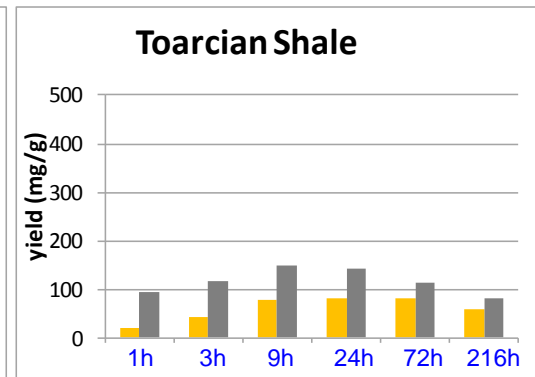
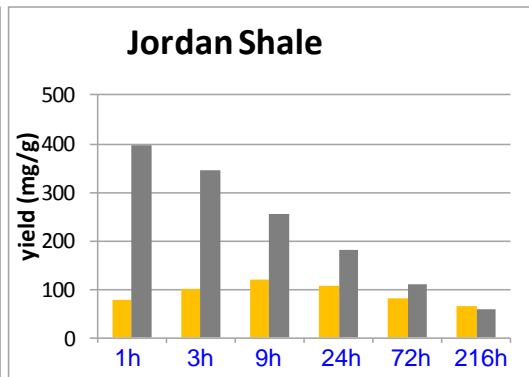
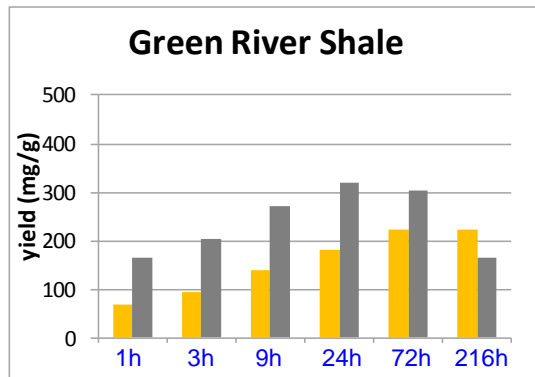


gas + liquid + solid > 95%

# Fluid composition during kerogen conversion

T = 325°C 1 to 216h

Kerogen conversion > 80% at 216h



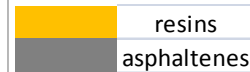
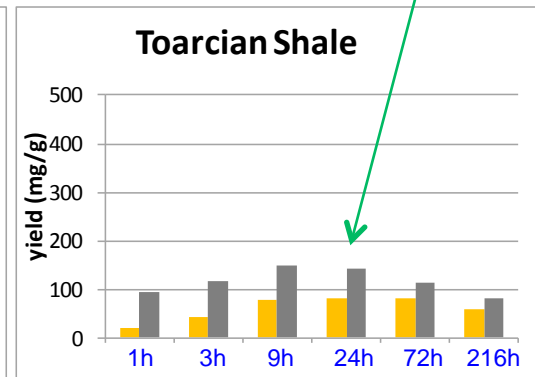
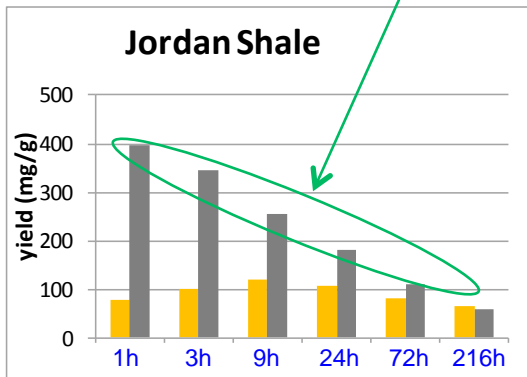
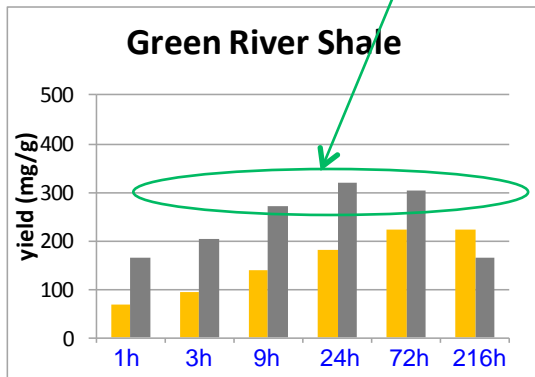
# Fluid composition during kerogen conversion

T = 325°C

Asp max : 300 mg/g  
Res max : 200 mg/g

Asp max : 400 mg/g  
Res max : 100 mg/g

Asp max : 150 mg/g  
Res max : 80 mg/g



**Total NSOs = 50%**

**Total NSOs = 50%**

**Total NSOs = 23%**

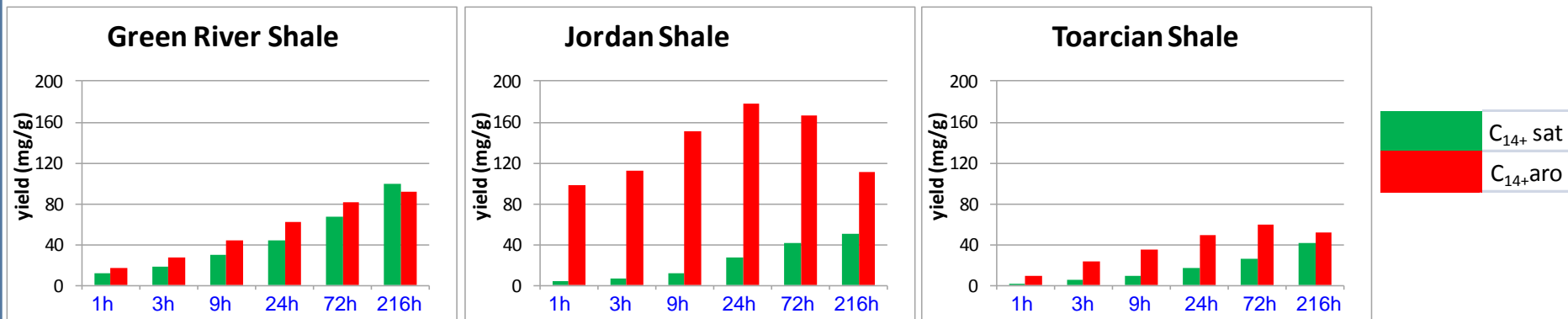
Asphaltenes : unstable class

Resins : more stable class



# Fluid composition during kerogen conversion

T = 325°C



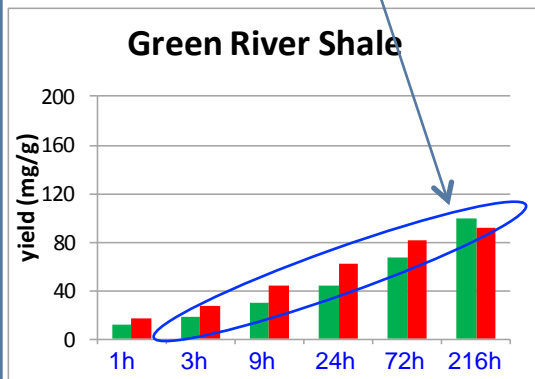
# Fluid composition during kerogen conversion

$T = 325^{\circ}\text{C}$

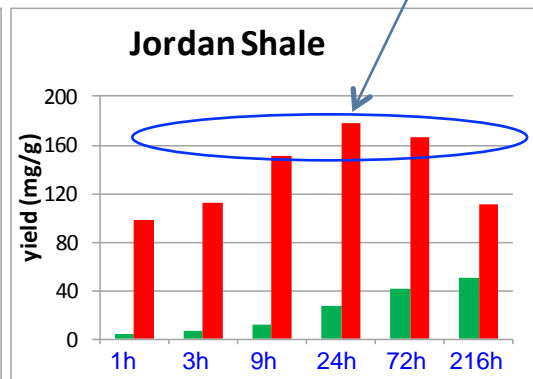
$\text{C}_{14+}$  Sat max = 10%  
 $\text{C}_{14+}$  Aro max = 9%

$\text{C}_{14+}$  Sat max = 5%  
 $\text{C}_{14+}$  Aro max = 18%

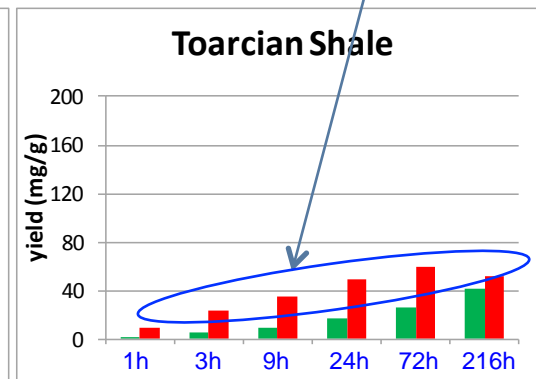
$\text{C}_{14+}$  Sat max = 4%  
 $\text{C}_{14+}$  Aro max = 6%



Total  $\text{C}_{14+}$  HC = 19%



Total  $\text{C}_{14+}$  HC = 23%



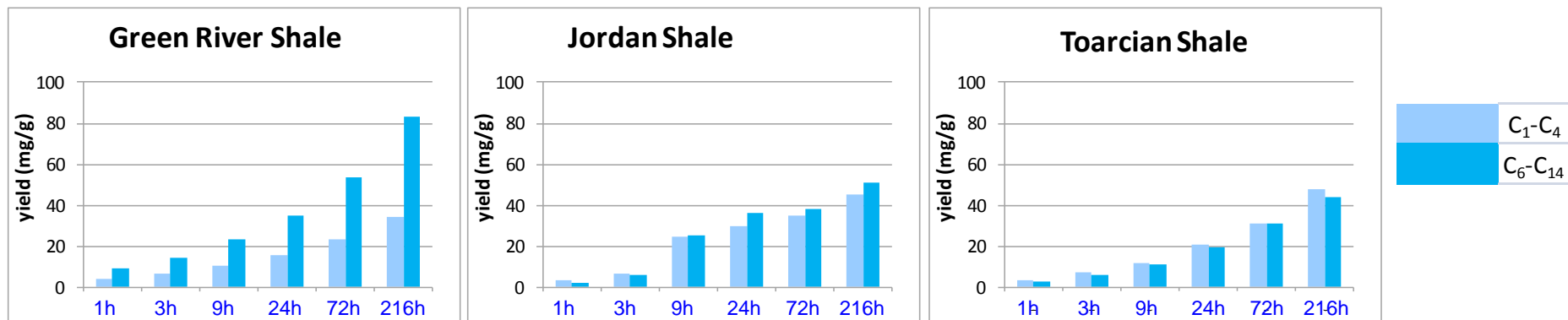
Total  $\text{C}_{14+}$  HC = 10%



$\text{C}_{14+}$  sat : almost stable  
 $\text{C}_{14+}$  aro : unstable

# Fluid composition during kerogen conversion

T = 325°C

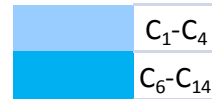
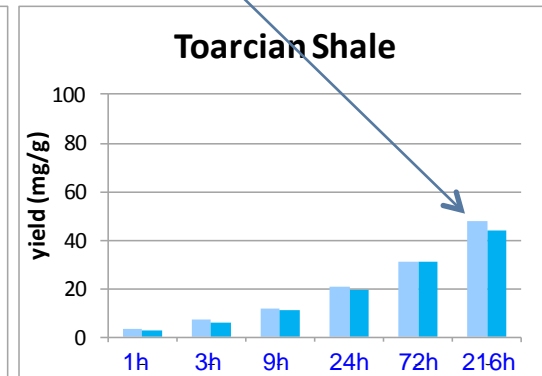
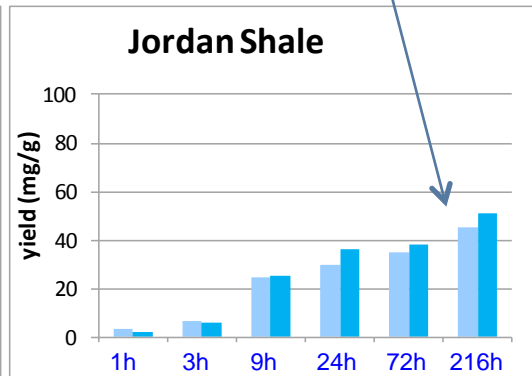
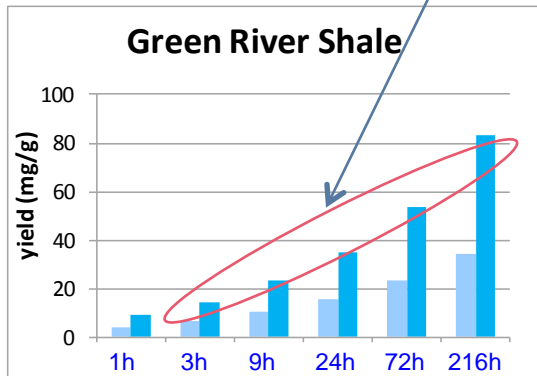


# Fluid composition during kerogen conversion

$T = 325^{\circ}\text{C}$

$\text{C}_1\text{-C}_4 \text{ max} = 4\%$   
 $\text{C}_6\text{-C}_{14} \text{ max} = 8\%$

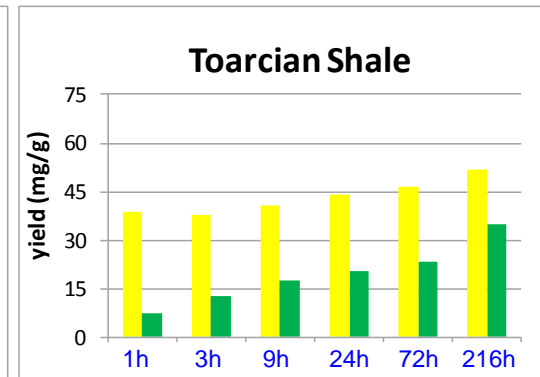
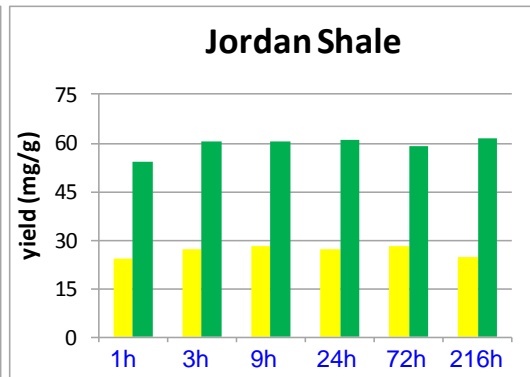
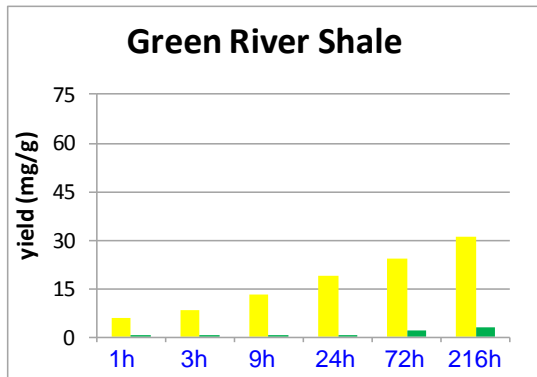
$\text{C}_1\text{-C}_4 \text{ max} = 4\%$   
 $\text{C}_6\text{-C}_{14} \text{ max} = 5\%$



Maximum  $\text{C}_6\text{-C}_{14}$  for the Type I kerogen

# Fluid composition during kerogen conversion

T = 325°C

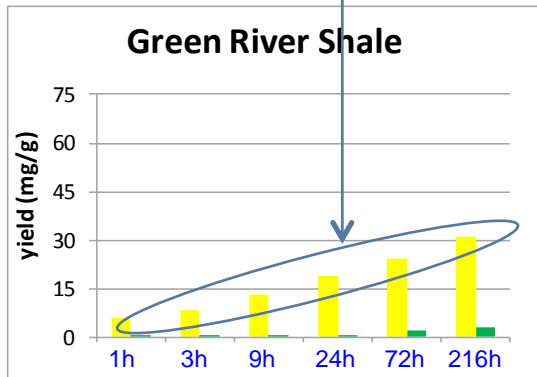




# Fluid composition during kerogen conversion

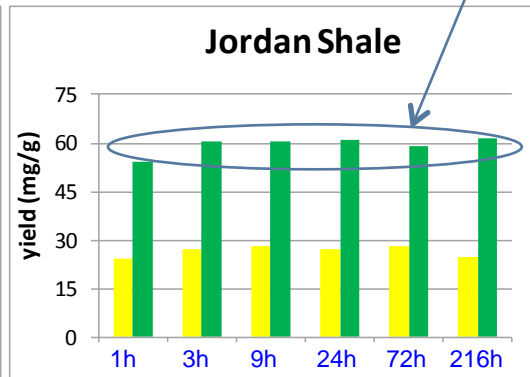
T = 325°C

CO<sub>2</sub> max : 3%  
H<sub>2</sub>S max : 0.5%



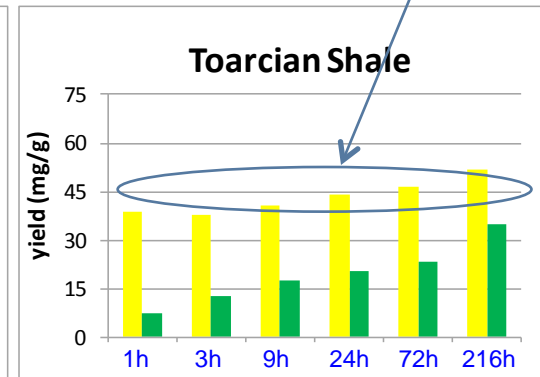
Total Acid gas = 3.5%

CO<sub>2</sub> max : 3%  
H<sub>2</sub>S max : 6%

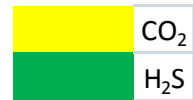


Total Acid gas = 9%

CO<sub>2</sub> max : 5%  
H<sub>2</sub>S max : 3%



Total Acid gas = 8%



Acid gas : very early generation

# Summary

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## ► **First step : kerogen cracking**

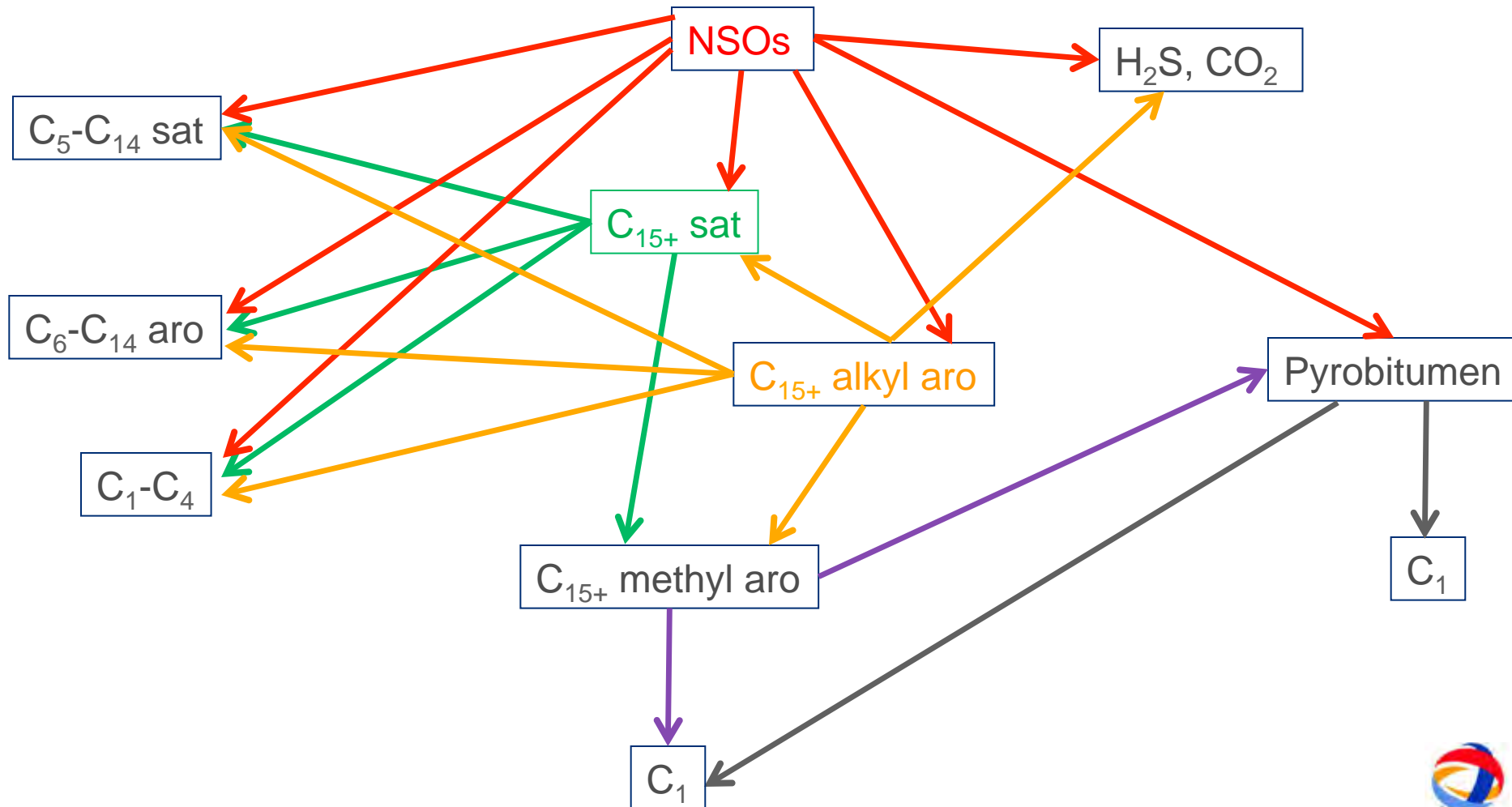
- Most of the asphaltenes are degraded
- Resins are more stable class
- C<sub>14+</sub> aromatics start to be cracked at high kerogen conversion
- C<sub>14+</sub> saturates are almost stable

Still high content in NSOs (asp + resins) : production of low °API and low mobility fluid, → significant secondary cracking reaction

## ► **Second step : influence of the secondary cracking reaction**

- Available compositional kinetic schema

# Compositional kinetic schema for NSOs and HC cracking



# Summary

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## ► **First step : kerogen cracking**

- Most of the asphaltenes are degraded
- Resins are more stable class
- C<sub>14+</sub> aromatics start to be cracked at high kerogen conversion
- C<sub>14+</sub> saturates are almost stable

Still high content in NSOs (asp + resins) : production of low °API and low mobility fluid, → significant secondary cracking reaction

## ► **Second step : influence of the secondary cracking reaction**

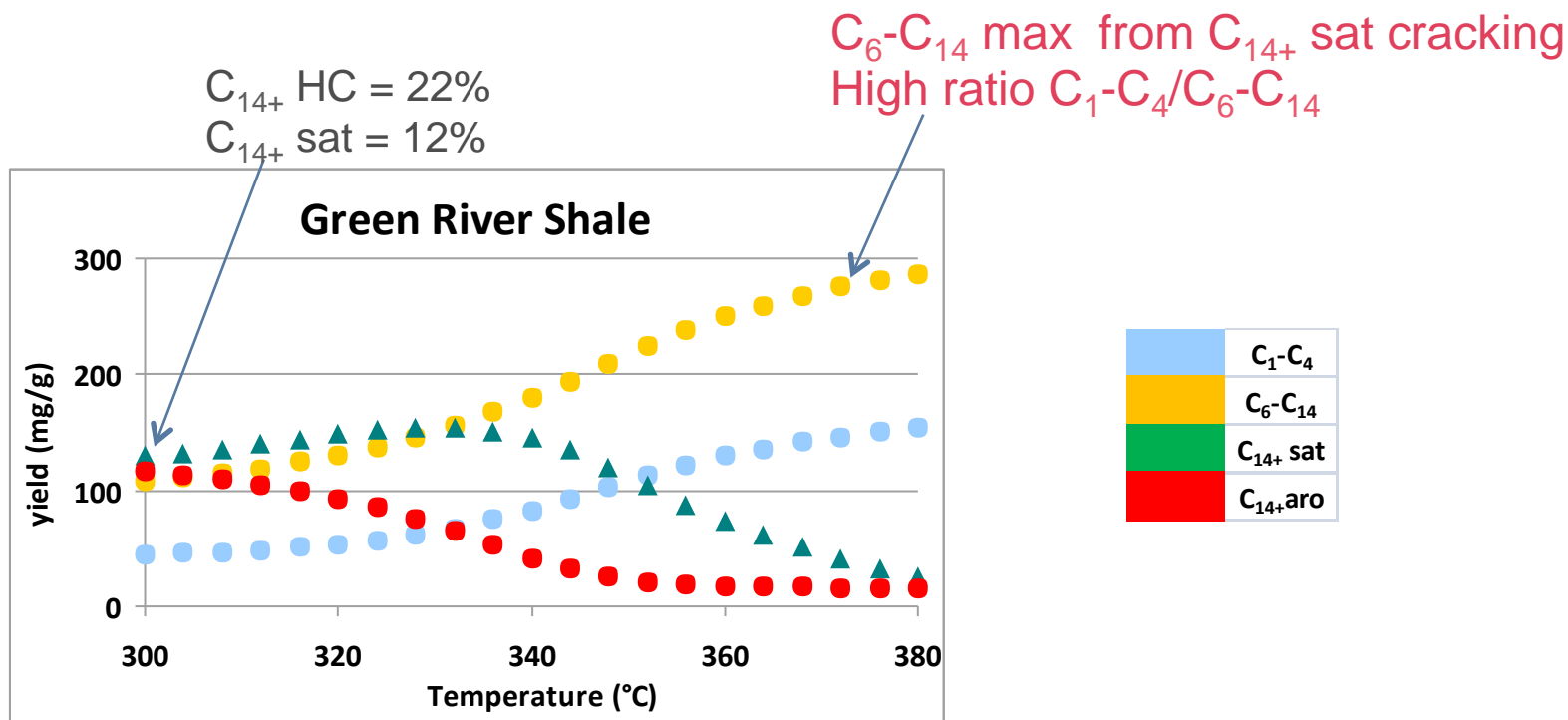
- Available compositional kinetic schema

→ Application to the fluid composition obtained at 325°C/216h

## Step 2 : thermal cracking of the generated products

### Kerogen conversion > 80%

T : 300 – 380°C at 4°C/day  
 Total duration : 3 months

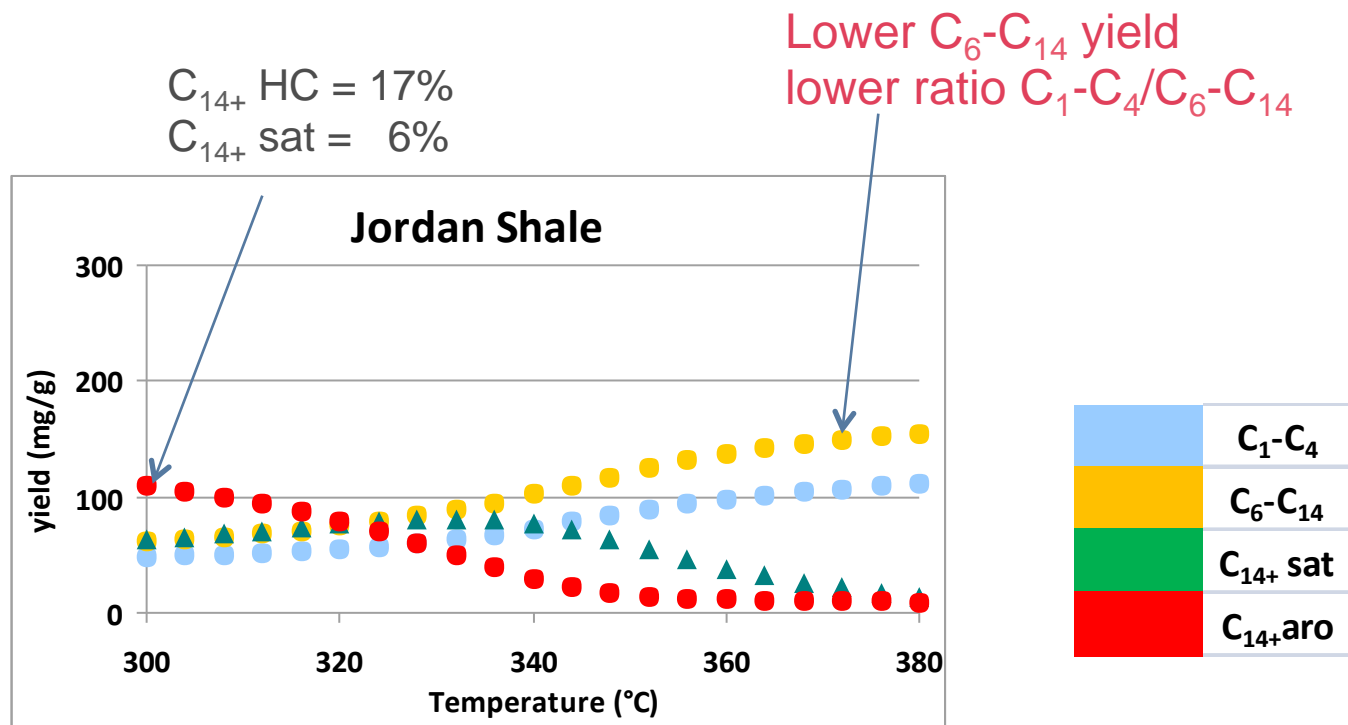


	$C_1-C_4$
	$C_6-C_{14}$
	$C_{14+}$ sat
	$C_{14+}$ aro

## Step 2 : thermal cracking of the generated products

### Kerogen conversion > 80%

T : 300 – 380°C at 4°C/day  
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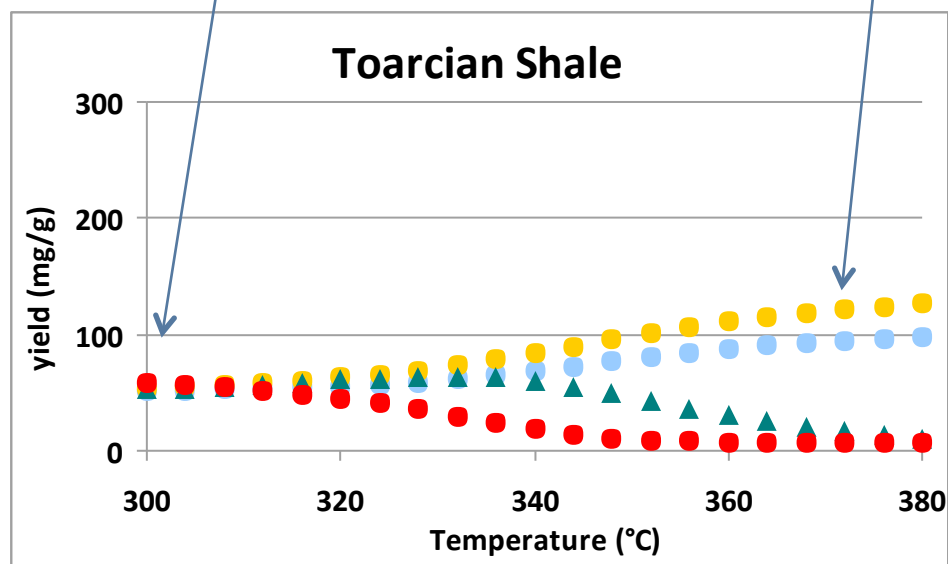
## Step 2 : thermal cracking of the generated products

### Kerogen conversion > 80%

T : 300 – 380°C at 4°C/day  
Total duration : 3 months

$C_{14+}$  HC = 12%  
 $C_{14+}$  sat = 6%

similar  $C_6-C_{14}$  as for the Jordan shale  
low ratio  $C_1-C_4/C_6-C_{14}$



# Conclusions : key geochemical parameters for optimizing oil shale process

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- ▶ **I – Organic matter type**
  - Best candidate : Lacustrine organic matter source
  
- ▶ **II – Organic carbon richness**
  - Best candidate : Lacustrine
  - Marine –S source rock
  
- ▶ **III – Good geochemical parameters**
  - Organic carbon richness : necessary but not sufficient
  - Low organic sulfur content
  - High asphaltenes and resins yield during pyrolysis
  - $C_{14+ \text{ sat}} / C_{14+ \text{ aro}} \gg 1$  in the generated hydrocarbons